7

Construction an innovative separator sunflower grain with new methods

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Abstract: The sunflower grain is very popular due to fresh and nutty consumption in some countries such as Iran, Turkey and many Arabic countries which is usually harvested without high capacity harvester at high moisture content in Iran. Also, the available methods have low efficiency for segregation the grains from sunflower head. Therefore, this study was conducted to design, construct and evaluate an innovative separator apparatus using the properties of nutty sunflower and applying kinematic equations. This apparatus includes the threshing and cleaning unit that the variables of its components are adjustable. So, with these capabilities, these variables can be optimized for any variety of sunflowers and this information can be used to develop suitable combine harvester. The experiments of evaluation and optimization designed using Response Surface Methodology (RSM) modeling method. The effects of rotational drum speed (380, 280, 180 rpm), feed rates (2000, 3000, 4000 (kg (head) h⁻¹), moisture content (60%, 45%, 30% w.b) for threshing unit, slope of sieves (0.12, 0.07, 0.02) oscillating frequency (7.6, 5.6, 3.6 Hz) and amplitude (25, 17.5, 10 mm) for cleaning unite were studied. Maximum and minimum threshing efficiency, separation efficiency and grain damage for threshing unit obtained 98.94% and 96.90%, 70% and 60.04%, 1.12% and 0.49% respectively. These results for cleaning efficiency and grain loss of cleaning unite reported 94.14% and 87.95%, 2.63% and 1.23% respectively. The result of ANOVA tables showed that the models were statistically significant at the 95% confidence level. The perturbation plots demonstrated that the moisture content had the greatest effect on threshing efficiency and grain damage followed by drum speed and feed rate. With decreasing the moisture content, threshing and separation efficiency increased and grain damage reduced. The oscillating frequency had more effect than other factors on cleaning efficiency, which with reducing it, the amount of cleaned grains increased. The optimized points were determined at the drum speed 376.634, feed rate 2000.06, moisture content 30, frequency 5.153, amplitude 25 and slope 0.02.

Keywords: nutty sunflower, separator apparatus, threshing and cleaning, RSM method

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1 Introduction

Sunflower (*Helianthus annuus L.*) is one of the most important oil crops in the world and is ranked 5th in oil production in the world (Chavoshgoli et al., 2015). Also, the edible sunflower is very popular due to fresh and nutty

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consumption in some countries such as Iran, Turkey and many Arabic countries. The nutty sunflower is harvested without combine or high capacity harvester at high moisture content in Iran (Mirzabe et al., 2014). It takes a lot of time and requires a large man power labour for removing the seeds from sunflower head. In general, there are two methods for removing sunflower seeds from the sunflower head, including 1) traditional manual method, and 2) mechanical mechanized methods (Mirzabe et al., 2016). The efficiency of the traditional manual methods is very low (Chavoshgoli, 2012; Mirzabe et al., 2016). The mechanical methods of removing sunflower seeds are based

on beating, friction and combination of them. Bansal and Dahiya (2001) studied the effect of threshing techniques on the quality of sunflower seeds. Sudajan et al. (2003) studied the effects of feed rate, type of drum and drum speed on sunflower threshing, they investigated power requirements and performance factors of a sunflower thresher and studied the effect of a number of drum characteristics on rasp-bar drum performance for threshing sunflowers (Sudajan et al., 2005). A local device for separating sunflower that would utilize both centrifugal and gravitational force was developed by Lotfy (2009). Ismail et al. (2009) optimized machine parameters of a pedal-operated sunflower threshing using friction drum. Aerodynamic and seed size, density, shape properties and friction coefficient are crucial properties in design and adjustment of combine harvesters, where usually a winnowing and sieving system is the first cleaning operation, followed by several (Munder et al. 2017). Fracture characteristics such as rupture force are dependent on most of the above named properties and are crucial for the design of threshing equipment (Thasaiya et al., 2014). Mirzabe et al. (2016) determined some physical properties of sunflowers head and studied effect of air-jet impingement parameters on the removing of sunflower seeds from the heads in static conditions. Azharuddin et al. (2016) designed and fabricated a machine which will separate the seeds from the head sunflower machine using peg tooth with an open threshing rotor and the performance of threshing machine is evaluated for its threshing efficiency, cleaning efficiency, visible damage seed, threshing capacity and specific energy consumption. According to researches, methods and devices developed in the field of separating and cleaning nutty sunflower grains from the point of view harvest capacity, separation efficiency and labor force have not been effective. Also, it is essential that apparent quality and marketability of this crop be desirable. Therefore, this study was conducted to design an innovative separator apparatus using the mechanical and physical properties of sunflower and applying the kinematic equations.

2 Materials and methods

2.1 Theory of Designing

For designing, the kinematic and dynamic studying on the components of apparatus and properties of crop was suitable method (Abdollahpour, 1998). For threshing of grain agriculture with drum thresher a power P_{th} (kW) is needed (Popov et al., 1986).

$$Pth = \left[\frac{q (aV - V1)}{(1 - f)}\right] V + AV + BV^{3}$$
 (1)

Where: q=feed rate (kg s⁻¹), V=linear speed of the drum (m s⁻¹), V_I =input speed of crop (m s⁻¹), f= the coefficient of friction, the A and B are coefficients of resistance that Popov et al. (1986) stated.

According to Sale et al. (2016) power required P_{cl} (kW) by oscillation mechanism is calculated as:

$$P_{cl} = \frac{Ws \times w \times 2y}{4500} + \frac{Ws \times w \times 2\mu \times 2x}{4500}$$
 (2)

Where, Ws =weight of sieve component along with threshed material (N), w=frequency of sieve oscillation (rad s⁻¹), μ =coefficient of friction of the moving component, x and y are horizontal and vertical displacement of the sieve (m).

With considering, that each beater of thresher receives equal mass of crop Q (kg) and rotational drum speed n (rpm), the number of beater N_b obtains as Equation 3 (Abdollahpour, 1998).

$$N_b = \frac{60q}{nQ} \tag{3}$$

The performance of the cleaning system depend on the scale of sieve, amplitude and frequency of oscillation, feed rate of crop, slope of the sieve, air flow rate and hole size of sieve, ratio amount of grain to MOG and properties of crop (Myhan et al., 2016). The following forces (Figure 1) act on a grain (m) lying on a sieve, with definite frequency w and amplitude r, effect on the cleaning and includes of: 1-weight of particle (G), 2- inertial force ($Pj = mr \ w^2 \ cos \omega t$), 3-The force generated by the air flow (R), 4-frictional force between the particle and the surface (f), 5- reaction force of the surface on the particle (N). In this regard, the Equations of 4, 5 and 6 obtained which state the motion of particles over the sieve surface at the delivery end. The sieves are set

inclined to the horizontal plane with the angle of α that should be smaller than the friction angle between the particles and the surface of sieve (φ) ($\alpha \le \varphi$).

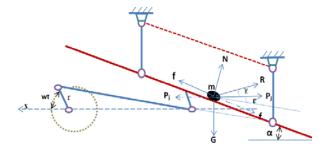


Figure 1 Forces action on a particle lying on a moving sieve and condition of sieves

$$\frac{rw_1^2}{g}cos\omega_1t = k_1cos\omega_1t > \frac{sin(\varphi\pm\alpha)}{cos(\varphi\pm\alpha-\varepsilon)} - \frac{R}{G}\frac{cos(\varphi\pm\alpha-\gamma)}{cos(\varphi\pm\alpha-\varepsilon)} \tag{4}$$

$$\frac{rw_2^2}{g}cos\omega_2t = k_2cos\omega_2t > \frac{sin(\varphi\pm\alpha)}{cos(\varphi\pm\alpha+\varepsilon)} + \frac{R}{G}\frac{cos(\varphi\pm\alpha+\gamma)}{cos(\varphi\pm\alpha-\varepsilon)} \tag{5}$$

$$\frac{rw_3^2}{g}cos\omega_3 t = k_3 cos\omega_3 t > \frac{cos\alpha}{sin(\varepsilon \pm \alpha)} - \frac{R}{G} \frac{sin(\gamma \pm \alpha)}{sin(\varepsilon \pm \alpha)}$$
 (6)

 $K(\frac{rw^2}{g})$, defines as a kinematic index and Iqbal (2006) stated that the normal working conditions for cleaner sticks as follows: $K_3 > K > K_1 > K_2$

K=2.2-3, r=23-30 mm, ε=12° 25°, α=1°-3° (few 7-8°), w=200-350 rpm.

The holes size using the geometric dimensions of the grains is calculated as (Chavoshgoli, 2012):

$$a_c \ge M_{av} + 3\sigma \tag{7}$$

Where, a_c =the holes size (mm), Ma=average of geometric dimension (including length, width and thickness), σ =the standard deviation of grain dimension.

2.2 Properties of crop

The nutty Sunflower heads with locale name of GALAMI variety were procured from sunflower farms of the Khoy city-Iran at moisture content of harvesting (Figure 2).

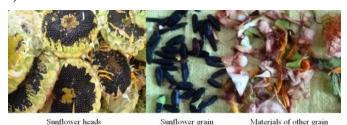
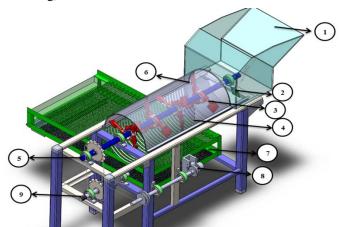


Figure 2 Grain and materials of other grain (MOG)

The energy required to rupture grain under quasistatic, which predicted grain behavior in dynamic loading and crucial impact velocity, estimated with an Instron Testing Machine (Model HOUNSFIELD-H5KS) (Selvam et al., 2014). Physical properties were calculated by methods of several other researchers (Chavoshgoli et al., 2015; Munder et al., 2017).

2.3 Description and designing of apparatus

The main components of apparatus for this research include the threshing unit (threshing drum and concave) and cleaning unit (sieves) that indicate in the Figure 3. The power required for applying the apparatus calculated from sum of Equations 1 and 3 that supplied by the tractor PTO (Model MF 285 with 55 kW power). The variables of performance are adjustable for any experiment. The factors that are considered for designing, Includes: diameter and rotational speed of drum thresher, length of thresher, structure, type and scale of concave (separator of threshing).



Threshing unit: (1) Input channel, (2) Feeder, (3) Beaters, (4)

Concave or separator, (5) Thresher shaft, (6) Covering of drum
thresher, -Cleaning unit: (7) set of sieves, (8) Crank of oscillation (9)

Power transmission

Figure 3 Schematic of the apparatus for separating sunflower grain

As shown in Figure 3, threshing unit operates on the principle of axial flow and combination of impact and rubbing sunflower heads is main reason to segregate grains from head in the condition of threshing. Set of beaters are installed with spiral pattern on the shaft thresher and number of them determined with regarding the Equation 3

and considering the capacity of feed rate. The soft and flexible material is selected for plates of beaters to prevent from grain damage (Qian et al., 2017). Angular position of plates is adjustable toward the shaft thresher which causes to progress the crops in the length of thresher. Diameter D (m) and rotational speed value n (rpm) determined using crucial impact velocity of grains and study of other researchers. In this study diameter of drum thresher is adjustable and maximum amount of it is regulated 0.6 m. The length of thresher was estimated by determining capacity and number of beater (Abdollahpour, 1998). The concave or separator was made of metal beams and the distance between these wires (separation grid) was determined by measuring the size of sunflower grains and MOG that were threshed. The feed rate of cleaning unit depends on the working capacity of thresher and length and

width of the sieve was determined using method of Abdollahpour (1998), per centimeter of drum thresher length, Surface area of the sieve is considered about 150-110 cm². For determining oscillation amplitude and frequency, the Kinematic Index $(\frac{rw^2}{g})$ was used. The size of sieve holes using Equation 7 and the slope of sieve (α) plate according to $(\alpha \le \varphi)$ was estimated.

2.4 Testing and evaluation of the apparatus

The variables, that have the greatest influence on efficiency, were determined for studying. The following performance indicators were used for the evaluation of thresher and cleaning unit (RNAM Test code, 1995): threshing efficiency%, separation efficiency%, cleaning efficiency%, grain damage% and grain losses% that calculated with method of Sudajan et al. (2005).

Table 1 Experimental design proposed by RSM for threshing unite

Std	Run	Run	Run	Run	A: Drum speed (rpm)	B: Feed rate (kgh ⁻¹)	C: Moisture content (w.b%)	Threshing efficiency(%)	Separation efficiency(%)	grain damage(%)
		(Coded value)	(Coded value)	(Coded value)	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •				
12	1	280 (0)	4000 (1)	60 (1)	97.03	57	1.1			
8	2	380 (1)	3000 (0)	60 (1)	98.73	57.33	1.12			
6	3	380 (1)	3000 (0)	30 (-1)	98.94	61.1	0.81			
7	4	180 (-1)	3000 (0)	60(1)	96.91	64.34	0.91			
4	5	380(1)	4000(1)	45 (0)	96.73	57.32	1.03			
3	6	180 (-1)	4000(1)	45 (0)	97.05	65	0.93			
15	7	280 (0)	3000 (0)	45 (0)	98.62	60.04	0.98			
1	8	180 (-1)	2000 (-1)	45 (0)	97.5	68.33	0.79			
16	9	280 (0)	4000(1)	45 (0)	98.19	60	0.87			
9	10	280 (0)	2000 (-1)	30 (-1)	98.87	70	0.58			
10	11	280 (0)	4000(1)	30 (-1)	97.98	62	0.61			
5	12	180 (-1)	3000 (0)	30 (-1)	98.1	64.68	0.49			
2	13	380 (1)	2000 (-1)	45 (0)	98.8	68	0.69			
11	14	280 (0)	2000 (-1)	60 (1)	96.9	66	1.01			
14	15	280 (0)	3000 (0)	45 (0)	98.85	62	0.86			
17	16	280 (0)	3000 (0)	30 (-1)	98.57	63.33	0.58			
13	17	180 (-1)	3000 (0)	45 (0)	97.7	65.98	0.68			

The developed threshing unit was evaluated against three threshing drum speeds of 380, 280, and 180 rpm, feed rates 2000, 3000, 4000 kg (head) h^{-1} and average moisture contents of 60% (moisture harvesting), 45% and 30% (w.b%). The testing of the cleaning unite was carried out to determine cleaning efficiency% and the grain loss% based on the slope of sieves ($\tan \alpha^{\circ}$) at levels of 0.12, 0.07, 0.02, frequency and amplitude of oscillation

at levels of 7.6, 5.6, 3.6 Hz and 25, 17.5, 10 mm respectively in the stable feed rate 3000 kg (head) h⁻¹ of threshing unit. The proposed experimental design by the Response Surface Methodology (RSM) method in design expert software 11 with Box-Behnken factorial design used (Tables 1 and 2) (Jamshidpouya et al., 2018). Also, the statistical analysis and optimization was performed with RSM method (Salari et al., 2013).

Table 2 Experimental design proposed by RSM for cleaning unite

		A': Frequency	B': Slope	C':Amplitude	Cleaning efficiency	Grain loss
Std	Run	(Hz)	(Without unit)	(mm)	(%)	(%)
		(Coded value)	(Coded value)	(Coded value)	(Coded value)	(Coded value)
2	1	7.6 (1)	0.02 (-1)	17.5 (0)	87.95	2.09
7	2	3.6 (-1)	0.07(0)	25 (1)	92.08	2.12
17	3	5.6 (0)	0.07(0)	17.5 (0)	89.55	2.03
1	4	3.6 (-1)	0.02 (-1)	17.5 (0)	92.26	1.7
10	5	5.6 (0)	0.12(1)	10 (-1)	93.16	1.9
12	6	5.6 (0)	0.12(1)	25 (1)	94.14	2.02
5	7	3.6 (-1)	0.07(0)	10 (-1)	89.12	2.41
6	8	7.6(1)	0.07(0)	10 (-1)	88.15	2.52
11	9	5.6 (0)	0.02 (-1)	25 (1)	91.44	1.63
14	10	5.6 (0)	0.07(0)	17.5 (0)	91.75	2.11
15	11	5.6 (0)	0.07(0)	17.5 (0)	91.34	1.93
3	12	3.6 (-1)	0.12(1)	25 (1)	93.35	2.33
13	13	5.6(0)	0.07(0)	17.5 (0)	88.15	2.57
8	14	7.6(1)	0.07(0)	25(1)	91.17	2.58
16	15	5.6(0)	0.07(0)	17.5(0)	91.35	1.96
9	16	5.6(0)	0.02(-1)	10(-1)	88.56	1.97
4	17	7.6(1)	0.12(1)	17.5(0)	93.7	2.21

3 Result and discussions

3.1 Properties of sunflower

The minimum and maximum energy required for grain rupture was recorded 26.26 and 35.1 mJ respectively. Also, the critical impact velocity according to Jafari et al. (2011), were calculated 12.48 and 14.77 m s⁻¹.

Table 3 Physical properties of nutty sunflower grain

properties	Minimum	Maximum	Mean	Standard deviation
Length, mm	18.4	35.46	25.84	0.14
Width, mm	6.12	13	9.3	0.06
Thickness, mm	2.9	9.19	4.99	0.047
Equivalent diameter, mm	18.14	14.16	10.93	0.055
Sphericity%	29.17	54.69	41.2	0.23
Mass, g	0.16	0.59	0.32	0.057
Project area, mm ²	91	239	137	0.29

Table 4 Physical properties of nutty sunflower grain and MOG

Properties	Minimum	Maximum	Mean	Standard deviation	
True density, kg m ⁻³	Grain	554	580	565	7.1
True delisity, kg ili	MOG	802	831	822	4.31
Dully dangites 100 mg-3	Grain	196	212	208	6.1
Bulk density, kg m ⁻³	MOG	81	99	89	3.08
D '40/	Grain	62.3	65.1	63.3	1.01
Porosity%	MOG	88.76	89.81	89.12	0.53
Dynamic angle of	Grain	21.1	22.7	21.9	0.4
repose	MOG	25.2	28.1	27.01	0.71
Coefficient friction	Grain	0.52	0.55	0.53	0.016
on steel surface	MOG	0.68	0.71	0.7	0.021
Terminal velocity, m	Grain	6.57	9.82	8.1	0.71
s ⁻¹	MOG	2.1	5.25	3.65	0.9
D	Grain	0.64	1.03	0.85	0.12
Drag coefficient	MOG	0.44	1.22	0.78	0.21

Table 3 and 4 shows the result of physical properties of grain and MOG at the moisture content of harvesting which it is need for designing and adjusting of apparatus variable in the condition of working.

3.2 Apparatus constructed for separation of nutty sunflower

The Figure 4 indicates constructed apparatus which has the ability to thresh, separate and clean the nutty sunflower crops and segregate grain from sunflower heads. It is an important step at development of sunflower combine harvester.



Figure 4 The constructed apparatus in the condition of working

The significance of each factor was determined using the F-test and p-value as shown in ANOVA Table. The corresponding variables would be more significant if the absolute F-value becomes greater and the p-value

becomes smaller (Safary and Chayjan, 2016). The ANOVA results, summarized in Table 5 and 6, showed that the model was statistically significant at the 95% confidence level. Statistical significance of the model, individual factors, their squares and interactions were estimated from their F-and p-values. The lack of fit was not significant relative to the pure error and meaning that the model was adequate for predicting performance of thresher and cleaner within the applied ranges of the process factors. The amount of F-value and P-value demonstrated more individual factors are statistically significant at the 95% confidence level for performance of apparatus, whereas interaction factor was not effective.

The perturbation plots compare the effects of all the factors at a particular point in the design space (Figures 5 and 6). A steep slope or curvature in a factor shows that the response is sensitive to that factor. As shown in Figure 5, the threshing efficiency, separation efficiency and grain damage are influenced by drum speed, feed rate and moisture content. Investigation the slope of plots (a and c) indicates that the moisture content had greatest influence in threshing efficiency and grain damage, as with increasing

the moisture content percentage of unthreshed and damaged grains increases. In high moisture contents, low threshing efficiency is due to more adhesion of grains on the sunflower heads which extra energy required for threshing, also the husk of grains is fragile in this condition that cause damaged grain. The Figure 5(b) illustrates which the separation efficiency increases with reducing of the factors. The sunflower heads with high moisture content are fragile and brittle, also in high drum speeds the number and amount of impact force applied to the crop rises, therefore the extra MOG that is produced and passes from separator, increases. Similar result was also reported by Goel et al. (2009). It is observed that curve slope of feed rate is steeper compared to other factors and has greater effect on the output of separator. The separation efficiency decreased by increasing feed rate, it is due to more and excessive collisions of heads with each other and rising the ratio of MOG to grain in the output of thresher. Maximum amount of the threshing efficiency, separation efficiency and grain damage 98.94%, 70% and 1.12% and minimum value 96.90%, 60.04% and 0.49% reported respectively.

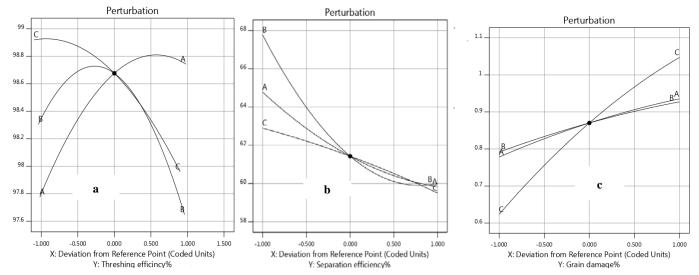
Table 5 Analysis of variance for performance of threshing unit using RSM

		•	-	8	8		
Source of variation	df -	Threshing Efficiency%		Separation Efficiency%		Grain damage%	
Source of variation	aı -	F-value	P-value	F-value	P-value	F-value	P-valu
Model	9	4.19	0.036	20.39	0.0003	4.69	0.027
Drum Speed(A)	1	8.44	0.0288	40.49	0.0004	4.4	0.074
Feed Rate(B)	1	4.49	0.0725	99.34	< 0.0001	3.29	0.1127
Moisture Content (C)	1	9.16	0.0192	18.96	0.0033	32.01	0.0008
AB	1	2.8	0.1383	10.18	0.0153	0.82148	0.396
AC	1	1.04	0.3407	0.188	0.1801	0.2465	0.634
BC	1	1.11	0.3273	0.677	0.6772	0.0733	0.794
A^2	1	2.71	0.1434	0.182	0.1822	0.0564	0.819
\mathbf{B}^2	1	8.31	0.0235	0.004	0.0042	0.0359	0.855
C^2	1	1.35	0.283	0.705	0.7056	0.3779	0.5582
Residual	7						
Lack of Fit	6	0.23	0.2355	0.742	0.7425	1.82	0.513
Pure Error	1						
Correlation total	16						

Table 6 Analysis of variance for performance of sunflower cleaning unit using RSM

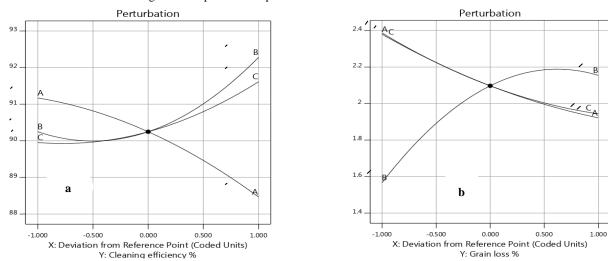
Source of variation	df	Cleaning Efficiency		Grain loss	
Source of variation		F-value	P-value	F-value	P-value
Model	9	3.75	0.0415	6.67	0.0102
Frequency(A')	1	10.74	0.0135	10.04	0.0158
Slope(B')	1	6.05	0.0435	16.55	0.0048
Amplitude(C')	1	4.63	0.0483	10.79	0.0134
A'B'	1	1.2	0.3091	0.0191	0.8939

A'C'	1	0.3476	0.574	6	0.0442
B'C'	1	0.0023	0.9627	2.06	0.1943
A'^2	1	0.5915	0.467	0.2978	0.6022
\mathbf{B}^{\prime} ²	1	3.31	0.1117	5.87	0.0458
C^{\prime} ²	1	0.8065	0.399	0.4259	0.5348
Residual	7				
Lack of Fit	6	0.1843	0.9019	0.2193	0.8785
Pure Error	1				
Correlation total	16				



(A) drum speed on the threshing efficiency; (B) feed rate on separation efficiency; (C) moisture content

Figure 5 The perturbation plots: effect of all the factors in thresher unite



(A'): frequency; (B'): Slope; (C'): Amplitude of Oscillation Figure 6 The perturbation plots: effect of all the factors in cleaning unite

The perturbation plots in Figure 6(a) showed that the slope of frequency curve was steeper than the slope of other factors and had more effect in cleaning grains on sieve. Also, with investigation the kinematic index $(\frac{rw^2}{g})$, this

conclusion is anticipated. According to Figure 6(a), the cleaning efficiency value increased with reduction of the frequency and increasing the slope of sieve and amplitude. The difference between the physical properties of grain and MOG (especially their density) is major reason in this result

that is effective in the movement and velocity of materials layers on the sieves. The Figure 6(b) illustrated the slope of the sieve had a greater effect on grain loss and with increasing it, the percentage of grains that removed from cleaner increased because the grains delivery to end sieve early and out with MOG. The increasing of frequency and amplitude of oscillation according to this study caused the reducing the percentage of grain loss, as the interaction of the grains increased and have further chance to pass through the holes. But excessive frequency increase is not recommended that causes grains being thrown on the sieve surface and do not through the holes. Maximum and minimum value for cleaning efficiency and grain loss reported 94.14% and 87.95%, 2.63% and 1.23% respectively.

3.3 Optimization of separator apparatus of grain sunflower

The multiple responses of design expert 11 used for finding the optimal point of the test variables, the desired goals (maximize or minimize) for each variable and response were chosen and different weights were assigned to each goal to adjust the shape of its particular desirability functions. Figure 7 display software generated optimum conditions of independent variables with the predicted values of responses for thresher and cleaner unite respectively. The goal of optimization is maximizing threshing and separation efficiency and minimizing of grain damage that the optimized values of variables such as drum speed 376.634 rpm, feed rate 2000.06 kg (head) h⁻¹ and moisture content 30% (w.b) were determined. Also the goal of optimization of cleaner is maximizing cleaning efficiency and minimizing of grain loss which the frequency 5.153 Hz, slope 0.02 and amplitude 25 mm were estimated.

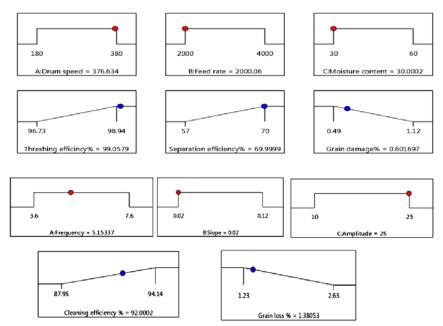


Figure 7 Optimized variables of cleaning unite

4 Conclusion

The separator apparatus of grain from sunflower head using properties of crops and kinematic equation was designed and constructed which had the capability of separation high capacity with adjustable variable as well as the development of machine harvesting. The ANOVA results of thresher and cleaner unites, showed that the

model was statistically significant at the 95% confidence level. The ANOVA and the perturbation illustrated the moisture content had greater effect than other factors on threshing efficiency% and grain damage%. Also, the feed rate of crops in thresher had the most influence in separation efficiency% and this result for cleaning efficiency% and gain loss% of cleaning unit was oscillating

frequency and slope of sieve. With decreasing the moisture content, threshing and separation efficiency increased and grain damage reduced. Decreasing the slope of sieve and oscillating frequency cause to rising cleaning efficiency and reducing grain loss. The optimized points were determined at the drum speed of 376.634 rpm, feed rate of 2000.06 kg (head) h⁻¹, moisture content of 30 (w.b), frequency of 5.153 Hz, amplitude of 25 mm and slope of sieve 0.02.

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