

# Validation of EGY-DRIP program in determining the optimum lateral length

Hisham Mohamed Imam<sup>1\*</sup>, Sabreen Khalil Pibars<sup>2</sup>

(1. *Department of Field Irrigation and Drainage Engineering Researches, Agricultural Engineering Research Institute, Giza, Egypt;*

2. *Water Relation and Field Irrigation Department, Agricultural Division, National Research Centre, El-Dokki, Cairo, Egypt.*)

**Abstract:** In drip irrigation systems the lateral lines are the pipes on which the emitters are installed. The accurate design of drip irrigation laterals needs to determine the total energy losses that include the pipe friction losses along the lateral line and minor losses due to emitter connections. A friendly user interface computer program named EGY-DRIP had developed for drip irrigation system design. The program had written in Microsoft visual basic 2013 to carry out hydraulic calculations of drip irrigation sub-unit design. The hydraulic calculation based on inputs of water properties, quality, soil characteristics, reference evapotranspiration, crop parameters, and irrigation system components (drippers, pipes, and fittings). The program supported with an upgradable Microsoft access database to facilitate data input by the user. The program determines the optimum lateral length applying two mathematical models developed using dimensional analysis. An experimental drip irrigation sub-unit was used to make a field evaluation of EGY-DRIP to determine the optimum lateral length for built-in and on-line emitters. The lateral length was determined on the base on 10% variation in the emitters' discharge, 50% friction head losses limit for manifold and 50% for the laterals. There was a good agreement between the field measured and the calculated optimum lateral length using EGY-DRIP program. The average difference between the measured and the calculated length was 0.5 m for built-in emitters and 0.58 m for the on-line emitters.

**Keywords:** validation, drip irrigation system, EGY-DRIP program, friction losses

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## 1 Introduction

Drip irrigation is one of the impotent modern techniques in irrigation systems which saves water, consumes low energy, improves the on-farm water management, and increases crop yield productivity. A typical drip irrigation system consists of the control head, main and sub-main lines, manifold, laterals, emitters, flow controls, and flow pressure regulators. For optimum design, the field divided into sub-units to reduce both pipelines diameters and lengths which in turn reduce the friction head losses, capital costs and to achieve better control of drip irrigation system.

Many considerations, which must be taken into account in the design of drip irrigation system, including field topography, soil type, crop to be grown, weather conditions, availability of labor, energy, available technology and financial resources. Attempts to quantify these parameters for designing drip irrigation systems resulted in a very cumbersome and time consuming task (Patel and Rajput, 2004). The use of computers removes much tedious work associated with repetitive complex calculations and manipulation of large pools of data. These results are in less error frequency and more detailed analysis when compared to non-computer aided design (Ismail et al., 2001).

Many of the developed computer models concerned basically the hydraulic design of lateral optimum length and commercial diameter by calculating friction losses and discharge that ensure emission uniformity (Martinez and Canales, 2009; Yurdem et al., 2011; and Nina et al.,

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\* **Corresponding author:** Hisham Mohamed Imam, Researcher. Department of Field Irrigation and Drainage Engineering Researches, Agricultural Engineering Research Institute, Egypt. Email: [hishamabokareem1973@yahoo.com](mailto:hishamabokareem1973@yahoo.com). Tel: +2011154333696.

2012). Some of these computer models exceeded to calculate pressure drop, flow rate and distribution uniformity of system pipelines network (manifold, sub-main and main lines) to find the economically optimum pipe size (Sharaf and Hassan, 2006; Zella et al., 2006; Ghaemi and Tabarzad, 2014). The design of a sub-unit was also considered in computer models through both size and shape of the irrigated area (Sharaf and Hassan, 2006; Mahrous et al., 2008; and Nina et al., 2012).

Model computations are supported by a database containing updated data of the micro-irrigation system components. Another database of crop properties, some Egyptian climatic zones and soil physical properties were utilized in designing computer models (Ismail et al., 2001).

Most of these developed models didn't concern the effect of the geometric parameters of emitters, soil physical properties, and irrigation water requirement on the determination of optimum length of lateral subsequently the dimensions and water distribution uniformity of sub-unit.

The objective is to evaluate the lateral length determination using EGY-DRIP computer program and to compare the simulated results with the on-farm measurements. EGY-DRIP program carries out hydraulic calculations taking into account data of water properties, the soil physical properties, the irrigation water requirement, and emitters geometrical parameters to determine the optimum length of the lateral and dimension of sub-unit.

## 2 Material and methods

The optimum lateral length determined by calculating the accumulated friction head losses between two adjacent emitters along the lateral line that variation in emitters discharge should not exceed 10%. The spacing between emitters in the row should not exceed 80% of the wetted diameter, which depends on the hydraulic conductivity of the soil, the emitter discharge, and on the total amount of water in the soil. It is useful to limit the lateral pressure head difference to 50% of the sub-unit pressure head variation and the other 50% to occur within the manifold (Keller and Bliesner, 1990).

### Wetted area:

Schwartzmass and Zur (1985) developed a general empirical equation to estimate the wetted depth and width (Keller and Bliesner, 1990):

$$w = 0.0094(z)^{0.35}(q)^{0.33}(k_s)^{-0.33} \quad (1)$$

where,  $w$  = wetted width or diameter of water pattern, (m);  $z$  = vertical distance to wetting front, (m);  $q$  = point-source emitter discharge, ( $L h^{-1}$ );  $k_s$  = saturated hydraulic conductivity of the soil, ( $m s^{-1}$ ).

### Emitter spacing:

Emitters might be placed on laterals to have an overlapping between adjacent wetted circles. The distance between two adjacent emitters is:

$$L=0.8w \quad (2)$$

where,  $L$  = distance between two adjacent emitters, (m).

### Emitter equation:

The relationship between emitter water discharge ( $q_e$ ) and operating pressure head ( $h_e$ ) is (Clark et al., 2007):

$$q_e = k_e h_e^x \quad (3)$$

where,  $k_e$  = Emitter discharge coefficient;  $x$  = Emitter discharge exponent;  $q_e$  = Emitter discharge ( $L h^{-1}$ );  $h_e$  = Operating pressure head (m).

### The allowable friction head losses difference:

The allowable difference in friction head losses of a sub-unit can be estimated using the following relation (Ismail et al., 2001).

$$\Delta H = x \left( \frac{\Delta q}{q} \right) \times h_{av} \quad (4)$$

where,  $\Delta H$  = allowable difference in friction head losses of a sub-unit (m);  $q$  = emitter discharge ( $L h^{-1}$ );  $\Delta q$  = allowable difference in emitter discharge ( $L h^{-1}$ );  $h_{av}$  = average operating pressure head of a sub-unit (m).

### Friction head losses model for lateral pipe with on-line and built-in emitters:

Two mathematical models were developed to predict the friction head losses between two adjacent emitters on lateral line equipped with both on-line and built-in emitters. The parameters affecting the friction head losses in lateral defined in dimensionless terms using Buckingham's  $\Pi$  theorem (Imam et al., 2015).

The predicting model of friction head losses in lateral line with on-line emitters is:

$$\Delta H = 0.498 \rho^{-0.152} \mu^{0.152} g^{-1} v^{1.848} D^{-1.468} L^{0.697} A_e^{0.309} \quad (5)$$

The predicting model of friction head losses with built-in emitters is:

$$\Delta H = 5.741 \rho^{-0.266} \mu^{0.266} g^{-1.734} D^{0.936} L^{0.141} D_e^{-1.158} L_e^{-0.185} \quad (6)$$

where,  $\Delta H$  = Friction head losses in emitter spacing (m);  $\rho$  = Water density ( $\text{kg m}^{-3}$ );  $\mu$  = Water viscosity ( $\text{kg ms}^{-3}$ );  $v$  = Average velocity ( $\text{m s}^{-1}$ );  $D$  = Inner diameter of the pipe (m);  $L$  = Emitter spacing (m);  $A_e$  = Barb protrusion area ( $\text{m}^2$ );  $D_e$  = Emitter inside diameter (m);  $L_e$  = Emitter length (m).

### Determination of lateral length:

Drip irrigation laterals are not only smooth pipes, but also have multiple outlets depending upon the emitter type and spacing. Since emitters discharge water along the lateral line, the total flow rate decreases and the pressure changes in the lateral line with respect to the length. For this reason, pressure and flow rate relations are considered in order to determine the optimum lateral lengths and water distribution uniformity from the emitters along the lateral Figure 1 (Yurdem et al., 2011). Starting from the far-end emitter, with the minimum desired discharge, moving against water direction, friction losses are calculated for each segment depending on the passing flow, which increases in the opposite flow direction (Alazba and El-Nesr, 2011).

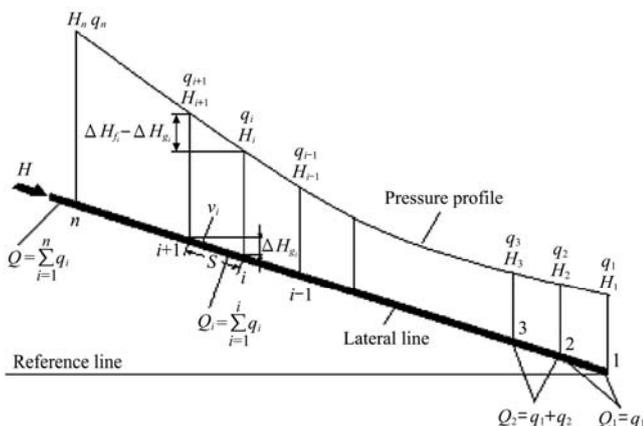


Figure 1 The pressure and flow rate distribution along the drip irrigation lateral line (Yurdem et al., 2011)

The inlet pressure head at every emitter expressed as (Yurdem et al., 2011):

$$H_i = H_{i-1} + \Delta H_f \pm \Delta H_g \quad (7)$$

where,  $H_i$  = inlet pressure in  $i$ th emitter (m);  $H_{i-1}$  = inlet pressure in emitter  $i-1$  (m);  $\Delta H_f$  = friction loss between emitter  $i$  and emitter  $i-1$  (m);  $\Delta H_g$  = elevation between emitter  $i$  and emitter  $i-1$  (m).

### EGY-DRIP program:

EGY-DRIP is a friendly user interface computer program developed to determine the optimum length of the lateral and the dimension of the sub-unit to achieve a high distribution uniformity of irrigation water. The program was written in Microsoft visual basic 2013. EGY-DRIP program carries out hydraulic calculations taking into account data on the soil physical properties, the irrigation water requirement, and emitters geometrical parameters.

The program uses both field and technical data to perform the hydraulic calculations. The user starts by entering field data about, water source and quality, soil characteristics, reference evapotranspiration, and planted crops. They needed technical data are specifications of drippers, distribution piping system and fittings. The program calculates the irrigation water requirements, number of drippers per plant, distance between drippers, optimum lateral length, and pressure head losses of manifold pipeline.

EGY-DRIP provided with a database for water quality, crops, reference evapotranspiration, and soil characteristics to facilitate input of data input by the user. The flow chart of the program is outlined in Figure 2.

EGY-DRIP program window are shown in Figure 3 which is contained:

### Menus:

There are only two pull down menus. File menu contains the basic functions of windows software like Open, Save, Print and Exit. The Database Update menu shows the database table to be updated.

### Side Tabs:

The tab control designed to be a platform for data input that is needed for the design process and hydraulic calculations. It contains tab pages of Project Data, Water Supply, Soil, Plant, Dripper, and Piping and Fitting.

### Tool Bar:

It contains buttons which trigger the calculation steps like irrigation water requirements, number of drippers, lateral and manifold friction losses. There is a button to present a printable form of the program outputs detailed report.

### Project window:

Project window represents the output of the design process and it contains of two tab pages outputs and

report tab page. The outputs tab page displays the results which are irrigation water requirements, dripper spacing, lateral design, manifold (length, telescopic diameters and friction losses) and sub-unit specifications. A graph area

was set aside to display the friction losses variation along the lateral length. The report tab page presents a printable copy of all project details and it can also be saved as text file.

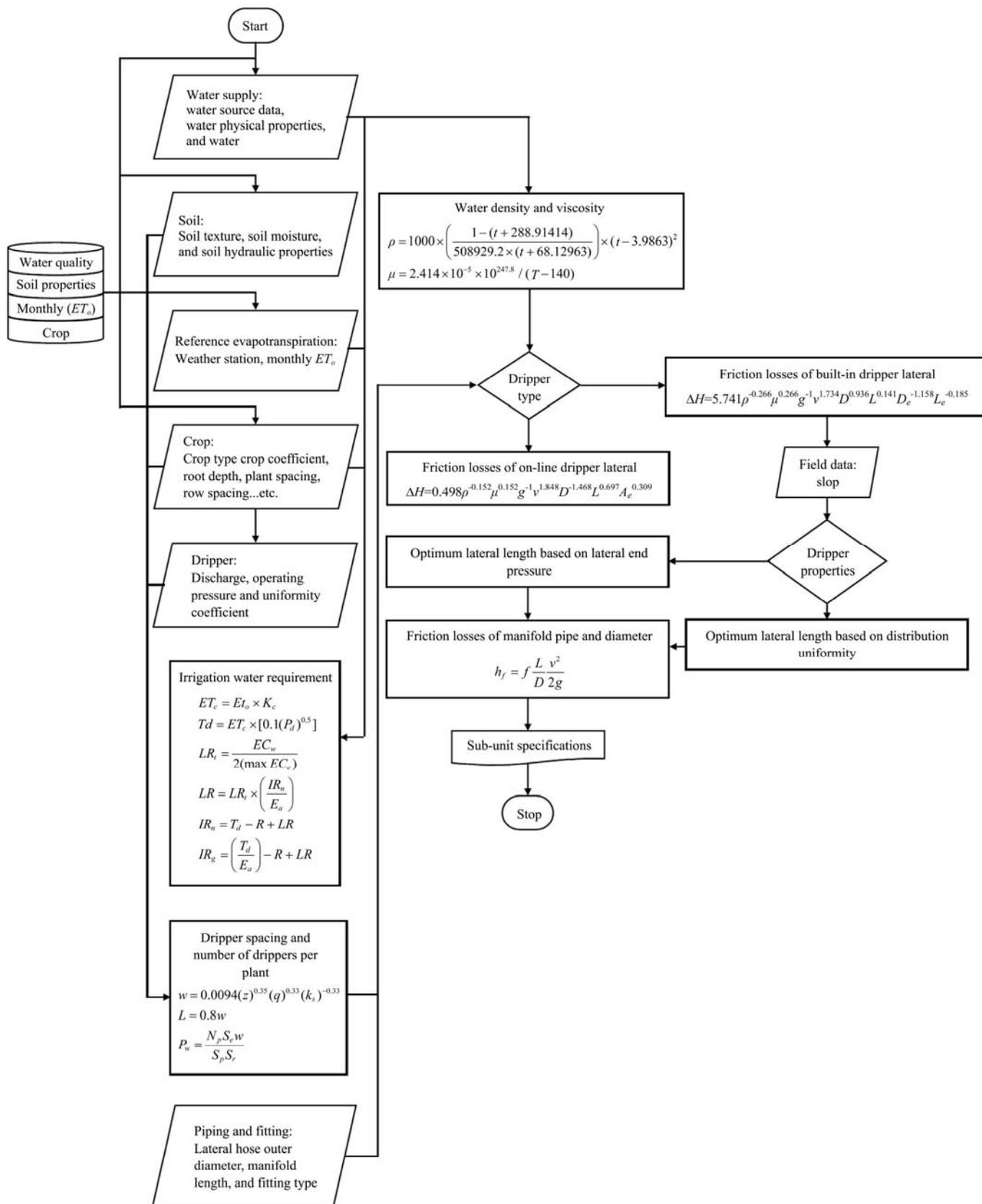


Figure 2 Flowchart of drip irrigation sub-unit design procedure using EGY-DRIP program



(a) Soil

(b) Plant

(c) Dripper

Piping and fitting

Figure 4 EGY-DRIP program data input tabs

**Table 1 The soil physical properties and mechanical analysis of the experimental site**

Depth (cm)	Physical properties						Mechanical analysis,%			
	SP (%)	$\theta_{Fc}$ (%)	$\theta_{wp}$ (%)	A.W (%)	BD (g cm <sup>-3</sup> )	HC (c h <sup>-1</sup> )	Course sand	Fine sand	Clay + Silt	Texture
0-20	21	10.1	4.7	5.4	1.69	22.5	47.76	49.75	2.49	Sandy
20-40	19	13.5	5.6	7.9	1.69	19	56.72	39.56	3.72	
40-60	22	12.5	4.6	7.9	1.67	21	36.76	59.4	3.84	

Note:  $\theta_{Fc}$  = Field Capacity,  $\theta_{wp}$  = Wilting Point, A.W = Available Water, and BD = Bulk density (g cm<sup>-3</sup>).

**Table 2 Crop parameters of Peanut (*Arachishypogaea L.*) cultivar Giza-6**

Crop factor		Value	
Mid-season crop coefficient ( $k_c$ )		1.15	
Depletion fraction		0.5	
Ground cover percentage (GC)		88	%
Wetted area percentage		70	%
Maximum root depth		0.75	(m)
Plant spacing		0.2	(m)
Row spacing		0.7	(m)
Salt tolerance ( $\text{minEC}_e$ )		0.4	( $\text{dS m}^{-1}$ )
Zero yield ( $\text{maxEC}_e$ )		0.8	( $\text{dS m}^{-1}$ )

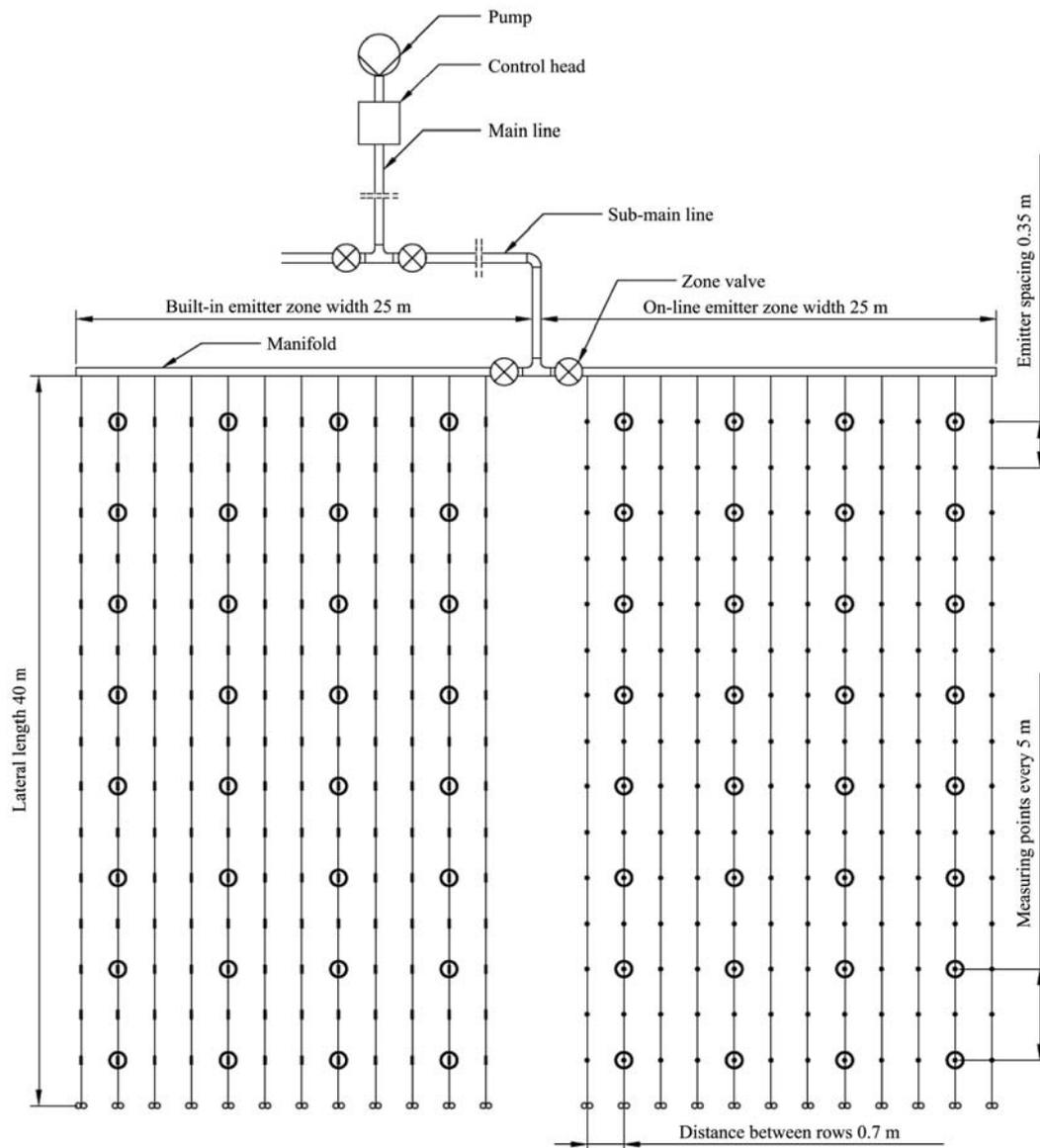


Figure 5 A schematic plan of measurement points for each emitter type, emitter spacing, and selected laterals

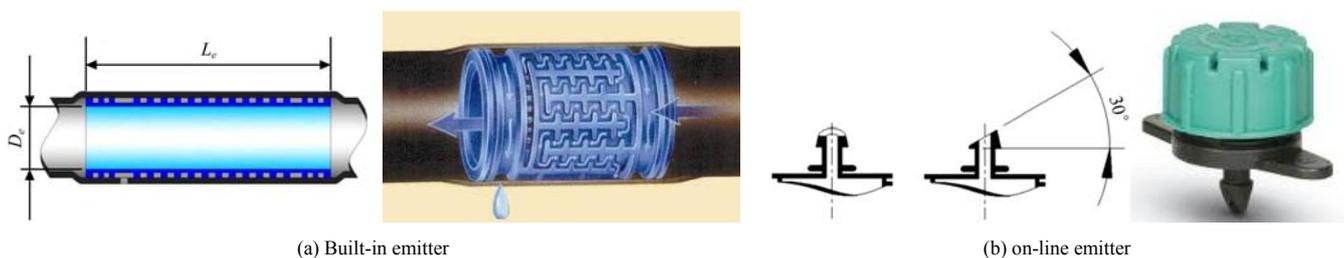


Figure 6 Types of the used emitters

**Table 3 Geometric and hydraulic specifications of both built-in and on-line emitters**

Specifications	Built-in Emitter	On-line Emitter
Emitter length ( $L_e$ )	35 mm	
Emitter diameter ( $D_e$ )	12 mm	
Emitter barb protrusion area ( $A_e$ )		13 mm <sup>2</sup>
Emitter discharge exponent ( $x$ )	0.537	0.548
Emitter discharge coefficient ( $k_e$ )	3.624	3.775
Emitter Coefficient variation (CV)	6.9%	5.7%

### 3 Results and discussion

#### Results:

The pressure drop along lateral lines of the experimental drip irrigation sub-unit was measured for both the built-in and on-line emitter types. The measured pressure drop and the discharge of the two emitter types are presented in Tables 4 and 5.

**Table 4 The on-field measurements of pressure drop and discharges of the built-in emitters along the selected laterals**

1st Lateral		2nd Lateral		3rd Lateral		4th Lateral	
$P$ (bar)	$Q$ (L h <sup>-1</sup> )	$P$ (bar)	$Q$ (L h <sup>-1</sup> )	$P$ (bar)	$Q$ (L h <sup>-1</sup> )	$P$ (bar)	$Q$ (L h <sup>-1</sup> )
0.97	3.912	0.97	3.9	0.96	3.804	0.95	3.648
0.97	3.888	0.97	3.912	0.95	3.72	0.94	3.6
0.97	3.864	0.97	3.84	0.95	3.696	0.94	3.612
0.97	3.84	0.97	3.816	0.94	3.6	0.92	3.492
0.97	3.852	0.96	3.78	0.94	3.564	0.92	3.444
0.96	3.732	0.96	3.72	0.91	3.48	0.91	3.324
0.96	3.708	0.94	3.624	0.9	3.456	0.9	3.276
0.92	3.468	0.9	3.384	0.86	3.3	0.84	3.18
0.88	3.384	0.86	3.288	0.82	3.24	0.81	3.12

**Table 5 The on-field measurements of pressure drop and discharges of the on-line emitters along the selected laterals**

1st Lateral		2nd Lateral		3rd Lateral		4th Lateral	
$P$ (bar)	$Q$ (L h <sup>-1</sup> )	$P$ (bar)	$Q$ (L h <sup>-1</sup> )	$P$ (bar)	$Q$ (L h <sup>-1</sup> )	$P$ (bar)	$Q$ (L h <sup>-1</sup> )
1.00	4.013	0.99	3.973	0.98	3.952	0.96	3.920
0.99	3.973	0.99	3.973	0.98	3.910	0.95	3.874
0.99	3.973	0.98	3.934	0.97	3.894	0.94	3.775
0.99	3.973	0.97	3.894	0.96	3.854	0.94	3.775
0.96	3.854	0.96	3.854	0.95	3.814	0.93	3.735
0.94	3.775	0.94	3.775	0.93	3.735	0.90	3.615
0.93	3.735	0.92	3.695	0.92	3.695	0.86	3.456
0.91	3.655	0.91	3.655	0.90	3.615	0.84	3.327
0.89	3.576	0.88	3.536	0.87	3.496	0.82	3.287

Data of water properties, soil characteristics, reference evapotranspiration  $Et_o$ , planted peanut crop parameters and the geometric dimensions of both built-in and on-line emitters were inputted to the EGY-DRIP program. The program determined the water density ( $\rho$ ) and viscosity ( $\mu$ ) through the water temperature. Both reference evapotranspiration  $Et_o$  and, planted peanut crop

parameters were used to calculate the needed emitter discharge ( $q$ ). To find the emitter spacing ( $L$ ), the program calculated wetted diameter which depends on saturated hydraulic conductivity of the soil and emitter discharge. The geometric dimensions of built-in were both the emitter length ( $L_e$ ) and inside diameter ( $D_e$ ), where it was barb protrusion area ( $A_e$ ) for on-line. The computer program calculated the expected friction head losses along the lateral line and the optimum lateral length by applying the mathematical models (5) and (6). The calculated optimum lateral lengths based on 10% variation in emitter discharge and 50% limit of pressure head losses for lateral. The calculated optimum lateral lengths using EGY-DRIP program were: 41, 41, 37, and 43 m for the built-in emitter and it was 36.25 m for the on-line emitters.

It can be noted from the on-field measured data in Tables 4 and 5 the measured optimum lateral lengths were: 40, 40, 38, and 38 m for the built-in emitters and 37.5, 37, 36, and 36 m for on-line emitters.

The statistical analysis showed no significant difference between the calculated and the measured lateral lengths for both built-in and on-line emitters. The f-ratio value is 0.157895 and P-value was 0.704853 as listed in Table 6. The result was not significant at  $P < 0.05$  for the built-in emitter lateral length.

**Table 6 ANOVA results of variation between the on-field measured and the calculated optimum lateral length by EGY-DRIP for built-in emitters**

Source of Variation	SS	df	MS	F	P-value	F crit
Between Groups	0.5	1	0.5	0.157895	0.704853	5.987378
Within Groups	19	6	3.166667			
Total	19.5	7				

The f-ratio value is 1.75 and P-value was 0.256435 as listed in Table 7. The result was not significant at  $P < 0.05$  for the on-line emitter lateral length.

**Table 7 ANOVA results of variation between the on-field measured and the calculated optimum lateral length by EGY-DRIP for on-line emitters**

Source of Variation	SS	df	MS	F	P-value	F crit
Between Groups	0.510417	1	0.510417	1.75	0.256435	7.708647
Within Groups	1.166667	4	0.291667			
Total	1.677083	5				

#### Discussion:

The comparison showed a good agreement between

the field measured optimum lateral length and that calculated using EGY-DRIP program for both built-in and on-line emitters. The average difference between the measured and the calculated length was 0.5 m for built-in emitters and 0.58 m for the on-line emitters. It could be due to the use of the mathematical models that developed by (Imam et al, 2015) using the dimensional analysis technique. The developed mathematical models to determine the friction head losses between two adjacent emitters concerning many parameters. These parameters are: water physical properties (density and viscosity), the distance between emitters (depends on soil hydraulic conductivity), the inner diameter of the lateral tube, emitters' discharge (depends on plant water requirement), and emitter's geometrical dimensions (barb protrusion area of on-line emitters and length and inner diameter of built-in emitters). EGY-DRIP program solves the developed models applying segment by segment technique that based on calculating the head losses due to friction between two adjacent emitters. Total lateral friction head losses is the summation of these segment pressure losses (Ismail et al., 2001). Calculation of friction head losses starts from the last emitter on the lateral line until the acceptable limit of pressure drop. The acceptable limit of pressure drop should not allow a variation in the emitters' discharge to exceed 10% by a lateral pressure head difference to 50% (Keller and Bliesner, 1990). Both the concerned parameters and solving technique resulted a relatively accurate determination of the lateral length.

#### 4 Conclusion

EGY-DRIP is a friendly user interface computer program developed to determine the optimum length of lateral and dimensions of sub-unit to achieve a high distribution uniformity of irrigation water. The computer program carries out hydraulic calculations to determine lengths and size of both laterals and manifold pipelines. The input data included water physical properties, water quality, soil characteristics, reference evapotranspiration, crop parameters, and geometrical parameters of both built-in and on-line emitters. The computer program used two mathematical models based on dimensional analysis developed to predict the friction head losses between two

adjacent emitters on lateral line and to determine the optimum lateral length equipped with both on-line and built-in emitters.

The result showed a good agreement between the on-field measured lateral lengths and the calculated lateral lengths using the computer program. The average difference between the measured and the calculated length was 0.5 m for built-in emitters and 0.58 m for the on-line emitters.

It is recommended to continue the development of EGY-DRIP computer program to have more functions and to be available on-line on the internet to cover a wider area of drip irrigation system designers and agricultural producers.

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