

A simulated effect of wetting and drying periods for two textural soils amended with biochar at a catchment scale

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Abstract: Biochar is considered as an option to ameliorate soil functions, by improving soil physical and hydraulic soil properties. This study investigated the effect of biochar and of wetting and drying cycles on the water infiltration at laboratory and at a hypothetical watershed scenario. In the laboratory, test samples with 2.5% and 5% (by dry mass) of a mango-wood biochar were added to a sandy and sandy loam soil material. Cumulative infiltration was determined after simulated intense wetting and drying cycles, by drying the samples at 30°C for three consecutive days. Additionally, biochar amended soil hydraulic parameters, obtained at the laboratory, were used to simulate the water discharge of a hypothetical watershed, with the Soil and Water Assessment Tool (SWAT). It was established that biochar addition and repeated wetting and drying cycles decreased cumulative infiltration and enhanced soil rigidity. At watershed scale, pore size distribution, in terms of hydraulic conductivity, played a key role to predict surface runoff and subsurface flow under fully and partially saturated conditions. These results contribute to understand better the effect of biochar amendments as a soil conservation management option on the watershed hydrology.

Keywords: infiltration, watershed, biochar, surface runoff, wetting, drying

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1 Introduction

Changes in the distribution, frequency and intensity of rainfall in combination with intensified soil degradation become a challenge to look for new forms of water management locally and at macro scale level. In agriculture, there is a need to look for new irrigation system

designs able to supply the crop water needs using less amount of water. On the other hand, drainage systems must be able to evacuate water properly under water excess and retain it under water scarcity. Regarding water scarcity, biochar has shown to enhance soil physicochemical and hydraulic characteristics (Abel et al., 2013; Ajayi et al., 2016) that may ameliorate soil water retention, nutrient and pollutant lixiviation and water transmissivity under adverse weather conditions.

Infiltration is an important function of the soil and acts as a control mechanism for surface runoff and groundwater recharge. Two forces matric as well as gravitational

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potentials— are in charge of moving the water flux from the surface into the soil profile. These forces produce, besides a downward movement, an upward and lateral movement (Baver et al., 1972) depending on the topographical conditions and the given anisotropy of the hydraulic functions. Initially, the water infiltration is high. When the soil is initially dry the hydraulic gradient as the sum of matric and gravitational potential dominates. At this stage, water infiltrates into the soil by capillary attraction as well as being pulled down by gravity but it fades off with time until it reaches a steady rate. As water penetrates deeper, it moves as a wetting front through the soil profile, the matric potential gradient decreases and the gravitational gradient becomes the only force that moves the water downward (Hillel, 1998; Jury and Horton, 2004). At this moment the flux tends to approach the hydraulic conductivity as a limiting value and the slope of the infiltration curve becomes flat. This steady condition is considered the maximum depth of water that can infiltrate the soil in a unit of time (Hillel, 1998). In the unsaturated zone, besides the main forces capillary and gravitational there are different mechanisms like absorption that helps to bind the water molecules to the soil bulk reducing the drainage of water into deeper layers.

Infiltration is influenced by many factors. Rainfall intensity and amount, drop diameter and drop size distribution may induce surface sealing, especially due to the raindrop impact, reducing permeability and slowing down infiltration (Assouline and Mualem, 1997). Soil texture, organic matter, structure and initial soil moisture content may alter the velocity at which infiltration occurs. Coarse soil textures are associated with high infiltration rates due to their larger pores and clay-rich soils are associated with lower infiltration (Chartier et al., 2011). For instance, studies such as from Adeniji et al. (2013) associated the soil fine fraction ($< 500 \mu\text{m}$) as a key factor to estimate infiltration. The latter soils however can also have a very high infiltration rate if they are well structured and if they have continuous coarse pores in the vertical direction. Organic matter, swell shrink processes amongst

others, all enhance soil structure and its strength and provide pores that are important for infiltration and water retention (Bens et al., 2007). High initial soil moisture may cause an early constant infiltration rate (Hillel, 1998). Vegetation stabilizes soil aggregates and is associated to nutrient conservation which is a positive effect for infiltration (Chartier et al., 2011). Finally, management practices such as tillage vary the composition of the top soil (Adeniji et al., 2013) enabling preferential flow (Hillel, 1998) or destroying macro pores (Nimmo, 2004) reducing water transmissivity.

Pore characteristics such as pore size distribution and connectivity, hydraulic conductivity and sorptivity are the most important parameters that influence infiltration capacity (Elrick and Reynolds, 1992; Jačka et al., 2016). Pore connectivity plays a key role by enabling the infiltrated water and solutes to reach deeper soil depths (Bens et al., 2007). Soils with high saturated hydraulic conductivity are associated with high infiltration rates (Hillel, 1998). Soil water repellency may delay initial infiltration rates with a later increase over time, due to air entrapment and flow instabilities (Bens et al., 2007; Carrick et al., 2011; and Dohnal et al., 2009).

Repetitive wetting and drying (WD) facilitate the formation of preferential flow paths (Peng et al., 2007) making the soil matrix sensitive to soil deformation and changing the configuration of structural pores which affect the transport of water and air (Dörner, 2005).

Biochar addition not only enhances processes such as soil water storage and conductivity, but it may also improve the soil infiltration capacity (Igbadun et al., 2016; Novak et al., 2016). Few studies have investigated the effect of biochar on infiltration and runoff formation. Itsukushima et al. (2016) reported higher initial and final infiltration rates in amended soils with bamboo charcoal and humus than in unamended soils. Hamidreza et al. (2016) indicated that the effectiveness of biochar in reducing surface runoff was influenced by the time of biochar application before the rainfall event, and suggested that the effect of biochar in the decrease of surface runoff resulted from increasing water

holding capacity or increasing infiltration capacity of the top soil. Hardie et al. (2011) and Doerr and Thomas (2000) suggested that hydrophobic soils affected the soil hydrology by producing a lower response in time to infiltration and accelerating time to runoff generation. Li et al. (2017) agreed on the benefits of agricultural and forest residues, in the form of biochar, on the decrease of surface runoff and its time of occurrence. Abrol et al. (2016) demonstrated that biochar is also useful as a soil conservation measure by ameliorating infiltration and controlling soil erosion.

Although many studies have pointed out the positive effects of biochar amendments on soil hydrology it still remains unclear what is the potential contribution of biochar as an agricultural management practice, especially under extreme weather conditions. The objective of this study is to investigate the effect of simulated WD on a hypothetical watershed assuming that the agricultural land is managed with only biochar application as an option for soil conservation. For the modeling of these hypothetical scenarios the soil hydraulic parameters of different biochar amendments, obtained at laboratory scale, were used as input parameters.

2 Material and methods

The present study was carried out in two parts: 1) Determining the water infiltration behavior at laboratory scale for different soil amendments applying simulated WD cycles; and 2) Evaluating a hypothetical watershed hydrological response, assuming the soil hydraulic parameters obtained at the laboratory scale for the same six

biochar amendment treatments.

2.1 Measurement of infiltration at laboratory scale

For the sampling preparation material from the A-horizon of two soils were used: a medium sand (S) from a Podsol derived from sandy outwash (99% sand) and a sandy loam (54% sand, 13% clay and 33% silt) from a stagnic Luvisol derived from glacial till (SL) collected in Schleswig-Holstein, in the northern part of Germany. The soil materials were air dried, homogenized and passed through a 2 mm sieve. As biochar, we added a pyrolyzed mango wood (600°C), with a mean particle size of 63 µm. at rates of 2.5% and 5% by dry mass. Six treatments were studied: S0 (control), S2.5 (sand + 2.5% biochar), S5 (sand + 5% biochar), SL0 (control), SL2.5 (sandy loam + 2.5% biochar) and SL5 (sandy loam + 5% biochar).

Soil cores of 100 cm³ with the homogenized soil were compacted to obtain average soil densities of 1.51 g cm⁻³ for the sandy mixtures and 1.39 g cm⁻³ for the loamy sand. Each treatment was prepared with three replicates. Infiltration capacity was first measured after sampling preparation (WD0), then oven-dried at 30°C for 72 h. Thereafter, infiltration capacity was measured again followed by an oven-dry period at 30°C for 72 h (WD1, WD2 WD3 and WD4). After each drying period, height changes were registered in order to quantify changes in bulk density. Moreover, weight of each sample was obtained to determine the initial soil water content. The sequence used for each WD cycle is depicted in Figure 1. All infiltration tests were performed under similar initial moisture conditions (~2 vol%). A WD cycle consisted of saturation during infiltration and thereafter oven-dry at 30°C for 72 h.

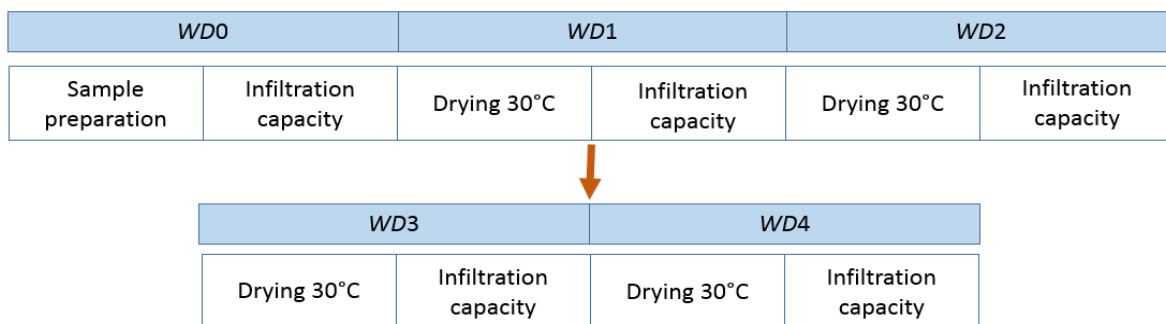


Figure 1 Simulated WD cycles to measure infiltration capacity

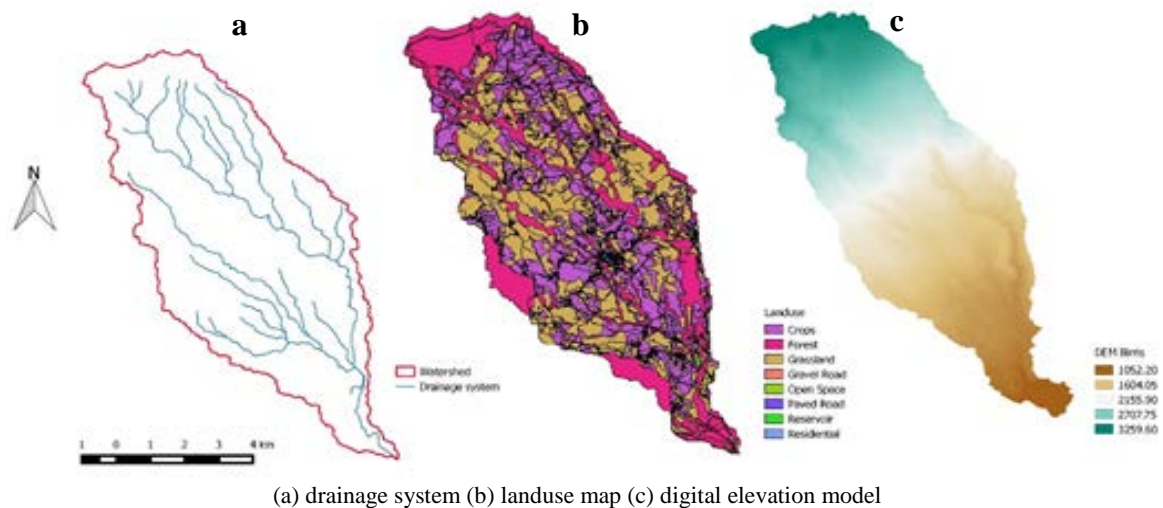
Infiltration rate was measured with a disk infiltrometer with an internal diameter (ϕ_i) of 23 mm. Time and water volume changes in the graduated disk infiltrometer were registered until volume changes reached a steady flow.

2.2 Macroscale modeling scenario with biochar amendments

2.2.1 Set of the geometry of the watershed

The geometry of the hypothetical macroscale scenarios was determined based on an elongated and sub-catchment

and youthful sub-catchment. The area of the watershed was set to 83.5 km² and occupied by 30% agriculture (crops) 39% cattle raising (grass land), 27% forest and 4% other uses such as residential areas and roads (Figure 2). It was assumed an average hillslope of 17% and a drainage system of order 4. With these characteristics we built a catchment with a quick response to rain events. Average annual precipitation was set to 2325 mm, a mean daily temperature value of 13°C and an average relative humidity of 88%.



(a) drainage system (b) landuse map (c) digital elevation model

Figure 2 Hypothetical watershed

2.2.2 Modelling main input parameters

The Soil and Water Assessment Tool (SWAT) version 1.5 (Dile et al., 2016) was used to model the catchment hydrology and to obtain the differences in surface runoff and water discharge at the outlet, for each treatment studied. SWAT is a physically based, long term yield model; and is used to predict the impact of land management practices on water, sediment and chemical yields (Neitsch et al., 2009).

Six scenarios were identified, sharing the same climate and land use data and differentiating only on the soil input

data (biochar amendments) for the areas occupied by Crops and Grassland, while in the other land use types (forest, residential and roads) soils were not amended with biochar. Thus, for these specific land use types six different soil conditions were set (based on the treatment sets for this study in Section 2.1) S0, S2.5, S5, SL0, SL2.5 and SL5. Six output scenarios, in terms of water discharge and surface runoff volume were obtained and discussed. Table 1 shows the main input model parameters based on the laboratory tests for layer 1 of the land use Crops and Grassland.

Table 1 Input model parameters, based on laboratory experiments, used to model the hydrological response of a hypothetical watershed

Land use type	Layer	Soil depth cm	Treatment	Hydrological group (CN)	K_{sat} mm h ⁻¹	ρ_d g cm ⁻³	AWC %	Biochar amount ton ha ⁻¹
Crops and Grassland	1	30	S0	A	613.33	1.50	30.00	-
			S2.5		143.33	1.50	53.00	112
			S5		70.00	1.50	69.83	225
			SL0	B	14.56	1.37	97.57	-
			S2.5		9.63	1.37	103.30	102
			SL5		5.28	1.36	108.87	204
	2	70	Clay loam	3.75	1.60	43.33		
	3	120		2.64	1.60	62.00		

Forest	1	30	A,B	16.88	1.05	55.50
	2	100		4.17	1.45	90.15
	3	133		4.48	1.65	42.09
Residential and roads	1	16	C,D	6.08	1.75	18.11
	2	46		2.21	1.80	32.68
	3	78		3.33	1.75	35.53

Note: CN: curve number; K_{sat} : saturated hydraulic conductivity; ρ_d : bulk density; AWC: available water content.

3 Results

3.1 Effect of wetting and drying (WD) cycles on water infiltration

Table 2 shows the cumulative infiltration at 45 minutes for all treatments, after applying the simulated (oven-dry) WD cycles. In all treatments, cumulative infiltration (I_{cum}) decreased as the biochar dosage increased. Data of I_{cum} for the unamended sand (S0) is not shown in this

table, since the infiltration test ran in a time shorter than 45 minutes. However, data from a shorter time (not shown in this paper) confirmed the same I_{cum} and pattern. For a same treatment, as the WD cycle was applied, I_{cum} tended, in all cases, to decrease. In the sandy treatments (S) the changes were more significant than in the sandy loam treatments (SL).

Table 2 Cumulative infiltration (cm) at 45 minutes for all treatments after applying different wetting and drying periods

Treatment	Wetting and Drying Period (WD)			
	0	1	2	4
S0	ND.	ND.	ND.	ND.
S2.5	32.72 ± 4.81	24.10 ± 1.68	18.38 ± 0.24	16.38 ± 4.57
S5	14.51 ± 2.46	12.50 ± 0.87	11.86 ± 0.16	11.01 ± 0.83
SL0	17.38 ± 1.14	13.52 ± 2.70	13.18 ± 0.59	12.45 ± 0.51
SL2.5	13.32 ± 1.10	10.64 ± 0.61	11.16 ± 0.62	10.34 ± 1.22
SL5	10.38 ± 0.28	9.63 ± 0.07	9.77 ± 0.31	9.59 ± 0.22

Note: S: sand; SL: sandy loam; ND.: not determined.

Table 3 presents the effect of the simulated WD cycles on the bulk density. As the WD cycles occurred, bulk density increased considerably in the unamended sand (S0) whereas in the sandy mixtures (S2.5 and S5) the opposite occurred. As biochar dosage increased, it was determined, by visual observation, that the amendments were able to swell during wetting (reducing bulk density) and during drying, the amendments did not shrink enough to produce the opposite effect. Thus, the net bulk density, of the sandy mixtures, along the WD cycles, tended to decrease but not

considerably. In the sandy loam mixtures (SL), bulk density did not vary as significantly as in the sandy mixtures and it oscillated along the different WD cycles.

Although bulk density decreased (especially in the sandy treatments) as the WD cycles occurred, cumulative infiltration decreased, too. Initial soil moisture was kept constant, about 2 vol%, for all treatments along the WD cycles, with the exception of WD0, which corresponded to the soil moisture content before applying any wetting/drying condition.

Table 3 Bulk density (ρ_d) and soil water content (θ) on the sandy (S) and sandy loam (SL) mixtures after each wetting and drying cycle (from Villagra-Mendoza and Horn, 2019)

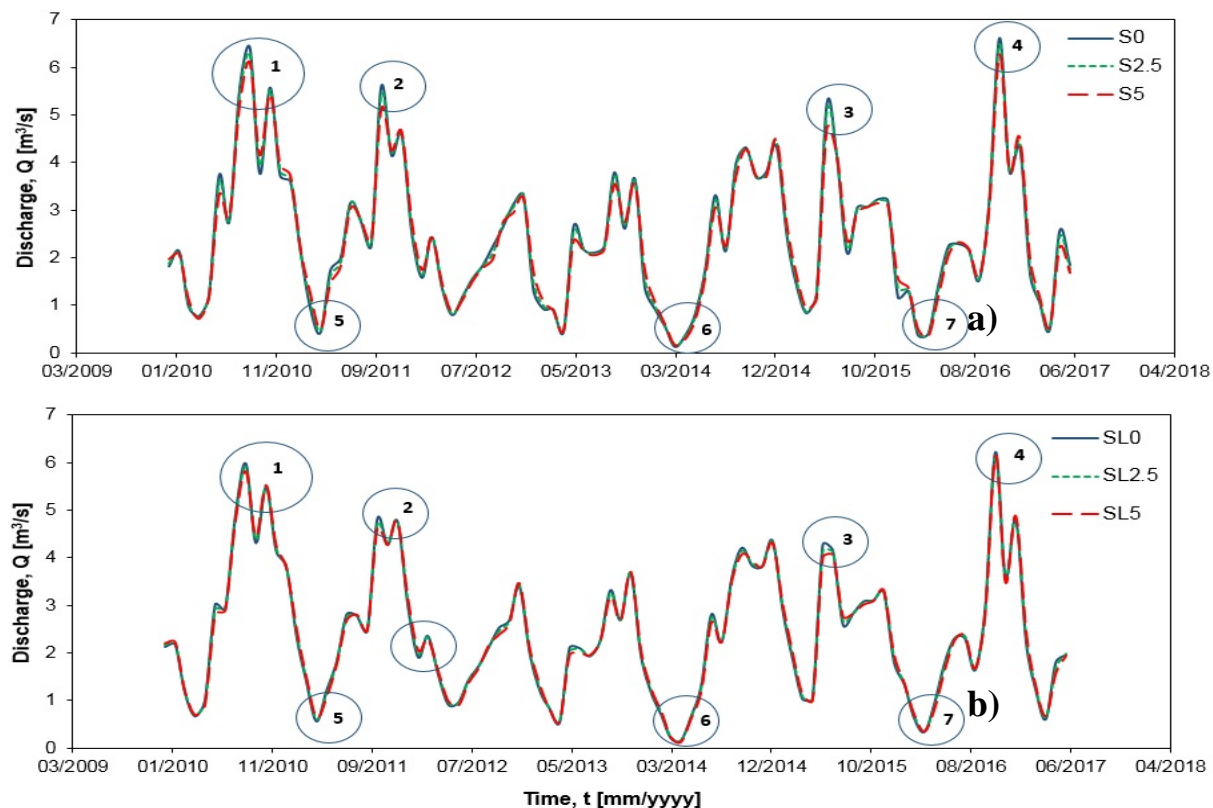
Treatment	Wetting/Drying Cycle (WD)							
	WD0		WD1		WD2		WD4	
	ρ_d	θ	ρ_d	θ	ρ_d	θ	ρ_d	θ
S0	1.55	1.3±0.54	1.54±0.03	1.1±0.45	1.61±0.07	1.2±0.46	1.71	1.0±0.43
S2.5	1.52±0.03	2.0±1.32	1.49±0.03	1.7±1.14	1.47±0.03	1.1±0.31	1.48	0.7±0.07
S5	1.48±0.01	1.7±0.31	1.46±0.02	1.1±0.28	1.46±0.02	1.1±0.21	1.43	0.8±0.09
SL0	1.38±0.02	4.6±0.72	1.36±0.02	1.8±0.10	1.37±0.01	2.1±0.17	1.38	1.9±0.05
SL2.5	1.40±0.05	5.5±0.86	1.39±0.06	1.9±0.04	1.38±0.05	2.4±0.12	1.35	1.6±0.08
SL5	1.40±0.04	5.2±0.79	1.36±0.05	1.9±0.11	1.35±0.02	2.3±0.11	1.37	1.9±0.07

Note: ρ_d : bulk density ($g\ cm^{-3}$); θ : initial soil moisture ($cm^3\ cm^{-3}$).

3.2 Hydrological response of a catchment with different biochar dosages

Because SWAT is a long-term hydrological model, the simulations referred to the response of the catchment to daily and monthly cumulative precipitation. Figure 3 illustrates the time series of the water discharge at the outlet of the model catchment for a period of 7 years. It is observed that the dry-season events (from November to April) produced significant smaller runoff peaks than the rainy-season events (from May to October). Figure 3a shows the time series of the water discharge (Q) for the

sandy amendments (S) and Figure 3b the time series corresponding to the sandy loam amendments (SL). The high peaks occurred during the rainy season and the low outflows during the dry season. For the sandy (Figure 3a) and sandy loam mixtures (Figure 3b) the catchment had the same water discharge shape, but the magnitude of Q varied, occurring a higher discharge in the sandy mixtures (S), mainly during the rainy season. Four high peaks during the rainy season (numbered from 1 to 4) and three low outflows during the dry season (numbered from 5 to 7) were chosen to compare the flow patterns.



(a) water discharge of the sandy treatments (b) water discharge of the sandy loam treatments

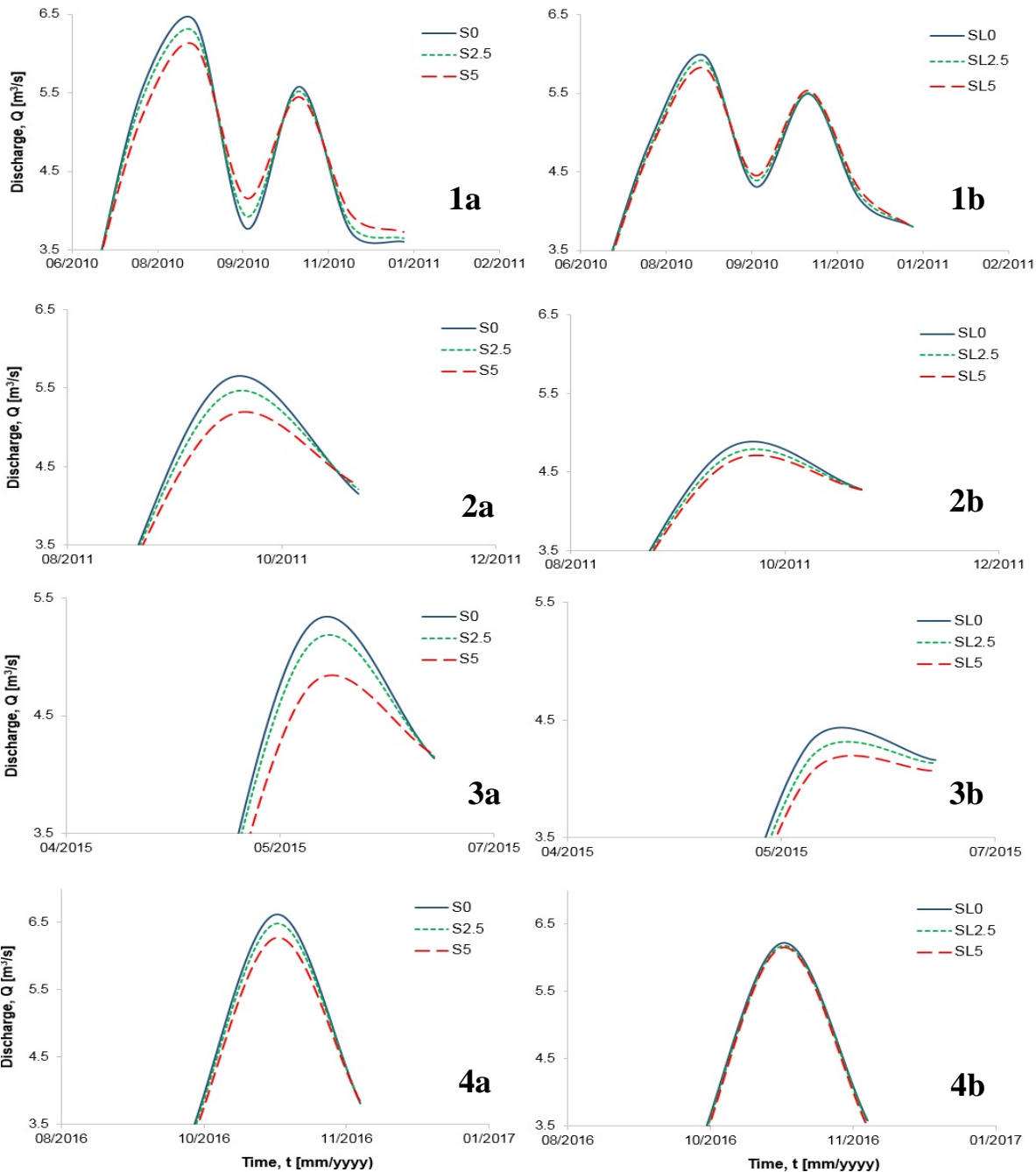
Figure 3 Simulated water discharge (Q) applying six scenarios (S0, S2.5, S5, SL0, SL2.5 and SL5) for the land occupied by Crops and Grassland

rainfall conditions. The sandy loam mixtures produced, on average, 10% less discharge (Q) than the sandy mixtures at the peak discharge events during the rainy season. This suggests that the sandy loam (SL) substrates were able to retain more water in the soil and transport less water within the soil bulk than the sandy (S) amendments, although they produced in general more surface runoff (Table 4). In the sandy treatments, the water discharge differences between the unamended sand (S0) and the amendments (S2.5 and

The circled high and low peaks are taken as examples for further analysis in Figure 4 and 5. Figure 4 shows the four examples of high peaks corresponding to the sandy mixtures (left) and sandy loam mixtures (right), during the rainy season (these discharge peaks are labeled as 1 to 4 in Figure 3). The unamended soils (S0 and SL0) had the highest discharge peaks with respect to their amendments. The sandy loam mixtures (SL) showed lower outflow peaks in comparison with the sandy treatments (S) for the same

S5) were more significant than the differences between the unamended sandy loam (SL0) and the sandy loam amendments (SL2.5 and SL5). Treatments S2.5 and S5 generated up to 7% and 20%, respectively, less water

discharge than the unamended sand, whereas, SL2.5 and SL5 produced up to 6% and 12% less water discharge than the unamended sandy loam (SL0).



(a) high peaks of water discharge of the sandy mixtures (S) (b) high peaks of the water discharge of the sandy loam mixtures (SL)

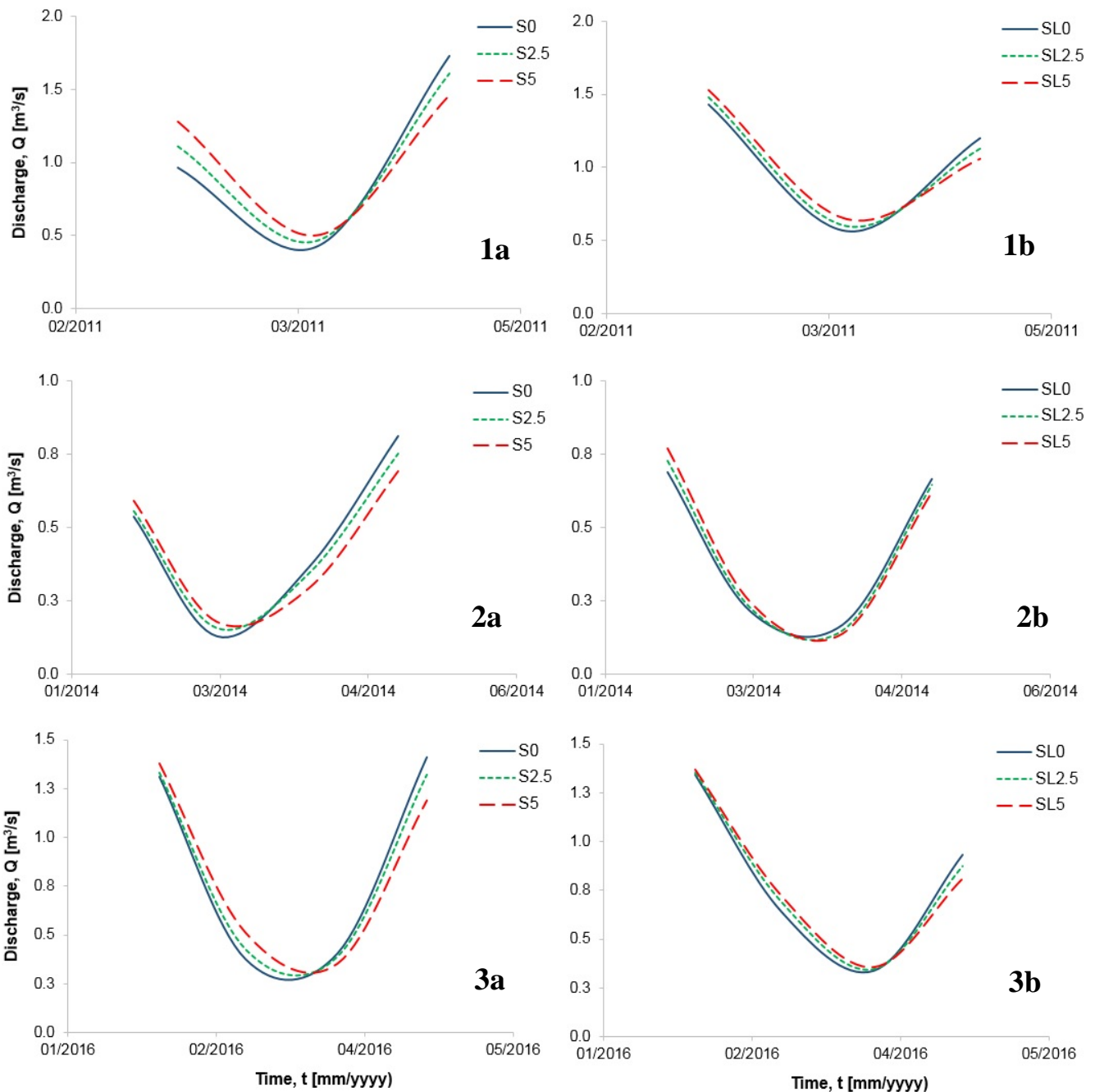
Figure 4 Comparison of four high outflow peaks Q for six scenarios (S0, S2.5, S5, SL0, SL2.5 and SL5) during the rainy season, for the land occupied by Crops and Grassland. Numbers follow the order in Figure 3

During the dry season (Figure 5), contrarily to the rainy season, the low outflows were higher in the sandy loam amendments (SL) than in the sandy treatments (S). On average, in the dry season the sandy loam mixtures (SL)

generated 21%, 18% and 14% more discharge with respect to the unamended sand (S0), and the sandy amendments with 2.5 (S2.5) and 5% (S5) biochar, respectively. This suggests that during the dry season, although precipitation

is low, the sandy loam mixtures continue contributing to the

drainage system greater than the sandy amendments.



(a) low outflow of the sandy mixtures (S) (b) low outflow of the sandy loam mixtures (SL)

Figure 5 Comparison of four low outflow peaks Q for six scenarios (S0, S2.5, S5, SL0, SL2.5 and SL5) during the dry season, for the land occupied by Crops and Grassland. Note: Numbers follow the order in Figure 3

Table 4 provides the average output values of the 1-D water balance parameters for the six soil scenarios. In overall, the sandy loam (SL) treatments produced more surface runoff than the sandy (S) treatments, whereas interflow (sub surface flow) was higher in the sandy treatments. The runoff coefficient (ratio of surface runoff

volume with respect to precipitation) was higher for the sandy loam mixtures (SL) reflecting high soil moisture conditions, whereas the interflow coefficient (ratio of interflow with respect to precipitation) was double the higher in the sandy treatments (S) than in the sandy loam substrates (SL). In average, the sandy substrates (S)

produced between 40% and 47% surface runoff volume from the total precipitation, whereas the sandy loam

mixtures (SL) produced between 28% and 33%.

Table 4 One-dimensional soil balance parameter values obtained from the simulated hydrological cycle using SWAT model, for six scenarios

Treatment	P	<i>Eva</i>	R	<i>Intf</i>	<i>CU</i>	Shallow aquifer	Deep GW recharge	R/P	<i>intf/P</i>
S0		536.0	168.69	769.1	12.77	460.04	24.85	8.6	39.0
S2.5		536.8	172.54	710.73	12.77	510.9	27.53	8.7	36.0
S5		538.7	178.36	612.67	12.77	596.47	32.03	9.0	31.1
SL0	1972.3	545.3	347.33	295.15	12.77	731.51	39.14	17.6	15.0
SL2.5		545.7	350.25	250.97	12.77	770.38	41.18	17.8	12.7
SL5		546.3	353.96	205.77	12.77	809.23	43.22	17.9	10.4

Note: P: precipitation; *Eva*: evapotranspiration; R: surface runoff; *intf*: interflow *CU*: capillary uprise; GW: groundwater. All parameters are in mm. R/P: runoff coefficient (%); *intf/P*: interflow coefficient (%).

4 Discussion

4.1 Effect of wetting and drying cycles on water infiltration

Bulk density and cumulative infiltration decreased for all treatments, except for S0. Usually, these two parameters show an opposite trend; however, bulk density as a capacity parameter may not be sufficient to explain the infiltration behavior (intensity parameter) and may lead to misunderstanding of the real mechanisms influencing water infiltration. If only bulk density is considered, only the changes on the mass per volume would be included, but not the effect of the connectivity nor the distribution of the pores that may also influence the water transmissivity within the bulk soil (Horn and Kutilek, 2009). Under these circumstances, intensity parameters such as hydraulic conductivity may explain better the decrease of I_{cum} over time. Saturated hydraulic conductivity values of the treatments studied for the different WD cycles (Villagra-Mendoza and Horn, 2018a) proved the pattern of I_{cum} , where a decrease of saturated hydraulic conductivity (K_{sat}), due to blockage of pores by biochar particles (Esmaelnejad et al., 2016; Masiello et al., 2014; and Novak et al., 2016), may cause a decrease of water infiltration, too. Porosity and the pore size distribution might have influenced the decrease of I_{cum} . Larger pores in the unamended sand (S0) were able to transport more water than narrow and medium pores, which were more frequent in the amended sandy soils and sandy loam mixtures (Villagra-Mendoza and Horn, 2018a) and the more frequent the narrow pores the lower the saturated hydraulic

conductivity was and the lower the cumulative infiltration. These results partially agree with findings of Ayodele et al. (2009) that reported that cumulative infiltration increased with a decreased bulk density, increased total porosity, sand fraction and saturated hydraulic conductivity. These findings are also contrary to the observations by Novak et al. (2016) of a packed sandy loam soil where biochar addition (pine chips) improved water infiltration but decreased after several infiltration events. It was suggested that water infiltration was affected by bulk density changes.

Githinji (2014) concluded that an increasing rate of biochar application produced a decreasing trend of cumulative infiltration in a sandy loam soil, and attributed this trend to biochar hydrophobicity. It was observed a linear decrease of K_{sat} with increasing biochar dosage, which also caused the reduction of the cumulative infiltration. Brockhoff et al. (2010) also described the decrease of K_{sat} as biochar dosage increased on a coarse-textured soil.

Wetting and drying cycles may also alter K_{sat} by changing the soil pore size distribution. Larger pores, in the unamended sandy soil, were more sensitive to deformation as shrinkage occurred and biochar ameliorated pore rigidity of the sand amendments. Soil rigidity may be interpreted as an enhancement of soil aggregation or greater void ratio values by means of narrower pores (Bodner et al., 2013; Horn et al., 2017; and Zong et al., 2014). The latter would be the result of macro pore instabilities, which decrease the ability of soil to transport water under saturated soil conditions. Ajayi et al. (2016) noted that in a sandy soil, K_{sat} tended to decrease as biochar dosage increased and the

number of WD cycles increased, attributing it to a micro-structural collapse of the soil bulk. Peng et al. (2007) reported that continuous intense WD cycles tended to decrease the void ratio of organic-rich soils, while in inorganic soils the void ratio increased. Zhao et al. (2015) observed that infiltration rate oscillated with different wet-dry cycles. It was reasoned that changes on macro porosity and near-saturated hydraulic conductivity were responsible for the same oscillation trend of water infiltration.

4.2 Effect of biochar amendments on the watershed hydrology

The unamended soils (S0 and SL0) discharged a higher water volume (Q) than the amended soils, with an increasing surface runoff and a decreasing subsurface flow (interflow) as biochar dosage increased. The increasing surface runoff was due to the decrease of the water infiltration as the biochar dosage increased. The processes behind these phenomena can be explained both by the reduced pore diameter due to the added biochar as well as by the increased water saturation or stronger menisci forces due to the smaller pore diameter (Hartge and Horn, 2016). Zhang and Hartge (1995) carried out infilling experiments and could prove the more pronounced strength but also altered water uptake rates. Thus, this study confirms the results of an increased field capacity and the range of the air entry value (Villagra-Mendoza and Horn, 2018b).

The decrease of interflow with the biochar addition may be related to the decrease of saturated hydraulic conductivity in the amendments. These results agree with findings of Lee et al. (2015) that observed a significant increase of runoff on biochar soil amendments compared to the unamended treatments. Others, such as Hamidreza et al. (2016) reported an amelioration of water infiltration in biochar amendments. Thus, the controversy results concerning the infiltration behavior maybe attributed and explained by the ageing effects for soils amended with biochar and the formation of soil aggregates which changes the infiltration capacity.

Under soil saturation conditions during the rainy season, the sandy loam mixtures (SL) showed less water discharge (Q) than the sandy mixtures (S). The runoff coefficient

(R/P) of the sandy loam treatments was higher than the coefficient of the sandy mixtures (S). In contrast, the interflow coefficient, in the sandy substrates, was approximately two times higher than the interflow coefficient of the sandy loam materials. This is explained by the effect of a multidimensional flow in the subsurface hillslope under in situ conditions, and a higher hydraulic conductivity in the sandy mixtures due to a greater amount of wider pores than in the sandy loam substrates (Villagra-Mendoza and Horn, 2018a). These findings also agree with observations of Imhoff and Akbar (2017), that reported a decrease of saturated hydraulic conductivity in an amended silt loam (30%) and sandy loam (54%) and an increase in a loamy sand (17%). They associated it with changes on the inter-pore volume, because small biochar particles filled the large pores between the sand particles, increasing the portion of finer pores.

Under partially saturated soil conditions (dry season) the sandy loam mixtures generated more water discharge (Q) than the sandy mixtures. When the soil is not completely dry the movement of water in the sandy loam is higher than in the sandy mixtures. This may be due to the higher available water content and more formation of narrow and medium pores in the sandy loam mixtures that increased the unsaturated hydraulic conductivity, enhancing the water flux under unsaturated soil conditions. After drainage of large pores and inter-particle pores occurs, water is retained in small pores and biochar intra-particle pore spaces. Thus, biochar increases water retention in the capillary region, which enhances the water transport under partially saturated soil conditions (Imhoff and Akbar, 2017). The more narrow and medium pores are formed due to biochar addition, the higher the unsaturated hydraulic conductivity (Villagra-Mendoza and Horn, 2018b). Imhoff and Akbar (2017) observed that when soil was not fully saturated, the unsaturated hydraulic conductivity was higher, due to an increase of the available water content in the loamy sand (70%) and sandy loam (20%), resulting in a less surface runoff.

5 Conclusion

1. Cumulative infiltration is not ameliorated with repetitive wetting and drying cycles.
2. The increase on unsaturated hydraulic conductivity of the amendments enhances the water transport during dry periods, although cumulative infiltration decreases.
3. Under dry soil conditions, biochar amendments are able to transport more water than the unamended soils, due to their higher unsaturated hydraulic conductivity.
4. Biochar amendment, as an option for soil conservation management, may help to improve water soil capacity under long dry conditions.

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